

TABLE I. Summary of plane-wave data for BaTiO<sub>3</sub> (5% CaTiO<sub>3</sub>).

| SHOT NO. | EXPLOSIVE                      | DRIVER              |                           |                         | NOMINAL SPECIMEN THICKNESS (mm) | FIRST WAVE <sup>a</sup>   |                           |                   |                    | SECOND WAVE                     |                       |                       |                   |                 |
|----------|--------------------------------|---------------------|---------------------------|-------------------------|---------------------------------|---------------------------|---------------------------|-------------------|--------------------|---------------------------------|-----------------------|-----------------------|-------------------|-----------------|
|          |                                | Material            | Thickness (cm)            | Press. (kbar)           |                                 | $U_1$ (mm/ $\mu$ sec)     | $u_1$ (mm/ $\mu$ sec)     | $\sigma_1$ (kbar) | $\rho_0/\rho$      | $U_2$ (mm/ $\mu$ sec)           | $u_2$ (mm/ $\mu$ sec) |                       | $\sigma_2$ (kbar) | $\rho_0/\rho$   |
|          |                                |                     |                           |                         |                                 |                           |                           |                   |                    |                                 | Imp. Match            | $\frac{1}{2} u_{fs2}$ |                   |                 |
| 7400     | P-40 <sup>b</sup>              | 2024 Al             | 1.25                      | 125 <sup>c</sup>        | 6                               | 6.15                      | 0.108                     | 37                | 0.982              | 4.74<br>4.89 <sup>d</sup>       | 0.56                  | 0.48                  | 144<br>149        | 0.898<br>0.901  |
| 7446     | P-60 <sup>e</sup> + 1" Baratol | 2024 Al             | 1.25                      | 133 <sup>c</sup>        | 3<br>12.5                       | --<br>6.15                | --<br>0.107               | --<br>37          | --<br>0.982        | --<br>4.76<br>5.18 <sup>d</sup> | --<br>0.6             | 0.56<br>--            | 154<br>167        | 0.8875<br>0.896 |
| 7447     | P-60 + 1" Comp B               | 2024 Al             | 1.25                      | 245                     | 3<br>6                          | --<br>6.32                | --<br>(0.11) <sup>f</sup> | --<br>(40)        | --<br>(0.982)      | --<br>5.82                      | 0.98<br>--            | 0.96<br>0.82          | 310               | 0.8363          |
| 8445     | P-60                           | Annealed Armco Fe   | 2.2<br>(6° taper)         | 7.9<br>131 <sup>c</sup> | 6                               | 5.25 <sup>g</sup><br>6.12 | 0.0175<br>(0.10)          | 5.1<br>(33)       | 0.9967<br>(0.9828) | --<br>--                        | --<br>--              | --<br>--              | --<br>--          | --<br>--        |
| 8748     | P-60 + 1" Baratol              | 4340 steel RC 30    | 4.6<br>(10° taper)        | 18                      | 5                               | 5.90                      | 0.0492                    | 16                | 0.9917             | --                              | --                    | --                    | --                | --              |
| 8882     | P-60                           | Brass + Lucite      | 1.25<br>1.2 (2° taper)    | 32                      | 6 (max)<br>10° wedge            | 6.15                      | 0.098                     | 34                | 0.9840             | --                              | --                    | --                    | --                | --              |
| 8883     | P-60                           | 4340 steel RC 50    | 3.2<br>(10° taper)        | 23                      | 5.4                             | 6.08                      | 0.065                     | 22                | 0.9891             | --                              | --                    | --                    | --                | --              |
| 8884     | P-60                           | 4340 steel + Lucite | 4.6<br>(10° taper)<br>0.6 | 2.5 <sup>c</sup>        | 6                               | 5.24                      | 0.016                     | 4.7               | 0.9969             | --                              | --                    | --                    | --                | --              |

- a. These data through Shot No. 7447 are approximate and not plotted in figures. This is because  $u_{fs}$  is not constant behind the first wave and its initial value was determined more precisely in wedge shots.
- b. A 4-inch explosive plane wave generator.
- c. Not measured, but assumed on basis of other shots.
- d. Determined from reverberation arrival, as in Fig. 4b. Only these points and Shot 7447 ( $U_2 \sim U_1$ ) are included in the figures.
- e. A 6-inch explosive plane wave generator.
- f. Most uncertain values indicated by parentheses.
- g. Apparent velocity of peak amplitude; near foot of wave, apparent velocity  $\sim 5.0$  mm/ $\mu$ sec.

in terms of wt%, were SiO<sub>2</sub> (0.32), Al<sub>2</sub>O<sub>3</sub> (0.30), SrO<sup>+</sup> (0.23), Na<sub>2</sub>O<sup>+</sup> (0.18), and P<sub>2</sub>O<sub>5</sub> (0.12). Purity of the calcium titanate additive is unknown. The mean densities of the bars were in the range 5.52 to 5.56 g/cm<sup>3</sup>, with about 1% variation within any given bar (density highest near surface). The longitudinal sound speed ( $c_L$ ) was found to be  $5.4 \pm 0.1$  mm/ $\mu$ sec at room temperature. The variation of  $c_L$  with temperature over a range including the Curie temperature (115°C) is shown in Fig. 1; the significance of these data will be discussed below. Figure 2 shows the results of static stress-strain measurements made at Sandia Corp.<sup>4</sup> These were nominally one-dimensional compressive stress experiments with  $\frac{1}{8} \times \frac{1}{8} \times 3$ -in. specimens; the strain was determined with a strain gauge cemented to the side of the specimen. The curves were terminated by shattering of the specimens.

The 95/5 PZT specimens were supplied in the form of circular disks, 2 in. in diameter by  $\frac{1}{8}$ - or  $\frac{7}{8}$ -in. thick, fabricated by hot pressing.<sup>5</sup> Their average densities ranged from 7.61 to 7.89 g/cm<sup>3</sup>, varying perhaps 1% in any given specimen (theoretical density is 8.16 g/cm<sup>3</sup>). Values of  $c_L$  ranged from 3.9 to 4.3 mm/ $\mu$ sec, generally increasing with density. A static stress-strain curve is included in Fig. 2.

<sup>4</sup> A. E. Binder (private communication).

<sup>5</sup> Supplied by Minneapolis-Honeywell, Minneapolis.

## EXPERIMENTS

The experiments were performed in two configurations, both of which have been described previously.<sup>6</sup> In one, a plane shock wave is produced in a specimen by means of an explosive plane-wave generator. In the other, an oblique shock wave is produced in a large specimen block by a detonation wave propagating in a thin sheet of explosive in contact with one face of the block. Shock velocities and particle velocities were deduced from shock arrivals and free-surface motion recorded with a smear camera. The polished ceramic reflected enough light from the argon bomb so that a metallic coating was unnecessary. The inclined mirror and optical lever techniques that were used have been described previously.<sup>6,7</sup> Examples of smear camera records from both types of shots are shown in Figs. 3 and 4.

Most of the low-pressure data for BT were generated in the oblique geometry; the advantage of this technique is that a range of pressures is covered in each shot. In particular, it is the most sensitive technique to study small variations of shock velocity with variations of shock amplitude. Of particular interest in the present work is a comparison of data from shots

<sup>6</sup> D. G. Doran, *High Pressure Measurement*, A. A. Giardini and E. C. Lloyd, Eds. (Butterworths Scientific Publications, Inc., Washington, 1963), p. 68.

<sup>7</sup> G. R. Fowles, *J. Appl. Phys.* **32**, 1475 (1961).

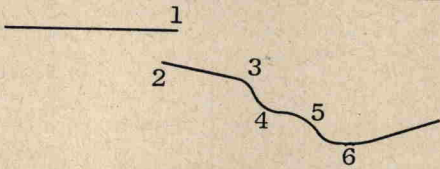


TABLE II. Summary of oblique geometry data for BaTiO<sub>3</sub> (5% CaTiO<sub>3</sub>). (Most questionable values indicated by parentheses.)  
(a) General shot data

| Shot No. | Specimen designation <sup>a</sup> | Wedge angle (°) | Explosive |                 |                     | Initial temperature (°C) | Initial density (g/cm <sup>3</sup> ) |
|----------|-----------------------------------|-----------------|-----------|-----------------|---------------------|--------------------------|--------------------------------------|
|          |                                   |                 | Type      | Thickness (in.) | Det. vel. (mm/μsec) |                          |                                      |
| 7396     | A                                 | 40°33'          | Comp B    | 0.188           | 7.86                | 20                       | 5.54±0.02                            |
| 7477     | C                                 | 25°29'          | Comp B    | 1.00            | 7.97                | 20                       | 5.54±0.02                            |
| 7540     | D                                 | 62°17'          | EL-506-D  | 0.017           | 7.31                | 17                       | 5.54±0.02                            |
| 7592     | Test-C <sup>b</sup>               | 64°30'          | EL-506-D  | 0.017           | 7.31 <sup>b</sup>   | 20                       | 5.54±0.02                            |
| 7612     | E                                 | 62°38'          | EL-506-D  | 0.017           | 7.37                | 21                       | 5.54±0.02                            |
| 8113     | J                                 | 70°47'          | EL-506-D  | 0.015           | 6.81 <sup>c</sup>   | 130                      | 5.53±0.02                            |

<sup>a</sup> Wedge dimensions 5x5x20 cm max., except No. 7592 (see note b).<sup>b</sup> Test wedge—from specimen block C. Maximum length = 10 cm. Detonation velocity assumed same as for Shot No. 7540.<sup>c</sup> Explosive also at 130°C.

## (b) Shot No. 7477



| First wave <sup>a</sup><br>(points 1-2) |                    |                      |               | Ramp <sup>b</sup><br>(points 2-3) |                    |                      |                      | Second wave <sup>c</sup><br>(points 3-6) |                    |                      |               |
|-----------------------------------------|--------------------|----------------------|---------------|-----------------------------------|--------------------|----------------------|----------------------|------------------------------------------|--------------------|----------------------|---------------|
| $U_1$<br>(mm/μsec)                      | $u_1$<br>(mm/μsec) | $\sigma_1$<br>(kbar) | $\rho_0/\rho$ | $U^* b$<br>(mm/μsec)              | $u^*$<br>(mm/μsec) | $\sigma^*$<br>(kbar) | $\rho_0/\rho_{av}^*$ | $U_2$<br>(mm/μsec)                       | $u_2$<br>(mm/μsec) | $\sigma_2$<br>(kbar) | $\rho_0/\rho$ |
| 6.35                                    | (0.096)            | (33.7)               | (0.9849)      | (5.5)                             | (0.129)            | (44)                 | (0.9790)             | (4.63)                                   | (0.515)            | (142)                | (0.895)       |
| 6.27                                    | 0.0887             | 30.8                 | 0.9859        | 5.3                               | 0.129              | 43                   | 0.9782               | 4.57                                     | 0.355              | 99                   | 0.929         |
|                                         | 0.0882             | 30.6                 | 0.9859        | 5.3                               | 0.127              | 44                   | 0.9782               | 4.54                                     | 0.368              | 102                  | 0.926         |
|                                         | 0.0898             | 31.1                 | 0.9857        | 5.3                               | 0.137              | 45                   | 0.9782               | 4.40                                     | 0.300              | 83                   | 0.937         |
|                                         | 0.0854             | 29.6                 | 0.9864        | 5.3                               | 0.135              | 45                   | 0.9782               | 4.33                                     | 0.327              | 90                   | 0.932         |
|                                         | 0.0876             | 30.4                 | 0.9860        | 5.3                               | 0.126              | 41                   | 0.9782               | 4.28                                     | (0.283)            | (78)                 | (0.938)       |
|                                         | 0.0854             | 29.6                 | 0.9864        | 5.3                               | 0.121              | 41                   | 0.9782               | 4.20                                     | 0.280              | 76                   | 0.938         |
|                                         | 0.0870             | 30.2                 | 0.9861        | 5.3                               | 0.128              | 42                   | 0.9782               |                                          |                    |                      |               |
|                                         | 0.0876             | 30.4                 | 0.9860        | 5.3                               | 0.118              | 39                   | 0.9782               |                                          |                    |                      |               |

<sup>a</sup> The first wave, ramp, and second-wave data do not correspond to the same positions on the wedge face.<sup>b</sup> The asterisks indicate effective quantities based on  $U^* = \frac{1}{2}(U_{a2} + U_{a3})$ , where  $U_{ai}$  is the apparent velocity of feature  $i$  of the trace, etc.<sup>c</sup> Jump 3-4 is due to the "reverberation" of the first wave (see text). Three discrete jumps were assumed in calculating the increase in free-surface velocity between points 3 and 6.  $U_2$  was computed from the average of  $U_{a5}$  and  $U_{a6}$ .

at 20°C with data from one shot at 130°C, above the Curie temperature of ~115°C. The experimental setup and smear camera record for the latter shot are shown in Fig. 4.

One oblique geometry shot was fired with a thick pad (1 in.) of explosive to obtain data on the two-shock profile.

All the data on 95/5 PZT were obtained in the plane-wave configuration.

## RESULTS

## Barium Titanate

Hugoniot data for BT are presented in Tables I and II and in Figs. 5-7. A two-wave structure is observed below 300 kbar, the highest point measured in this study. The first-wave amplitude is ~30 kbar and the velocity is ~6.27 mm/μsec.<sup>8</sup> These values are from the

<sup>8</sup> Corresponding values for "pure" BaTiO<sub>3</sub> are 25 kbar and 5.90 mm/μsec. (See Ref. 2.)

oblique wave experiments and are considered more accurate than those from plane-wave shots. This is particularly true of the first-wave amplitude because the stress and particle velocity continue to increase behind the essentially discontinuous wavefront, and hence it is difficult to measure the *initial* free-surface velocity accurately with the inclined mirror technique. The highest first-wave amplitude measured was 35 kbar, and there is a suggestion of shear stress relaxation<sup>9</sup> as the first wave propagates, i.e., the first-wave amplitude decreases somewhat with propagation distance in the presence of a following second wave.

The calculation of states behind the second wave is less straightforward than for the first wave because the second wave arrives at the free surface only after it has interacted with the reflection(s) of the first wave from the free surface. For two plane-wave shots (Nos. 7400 and 7446), the free-surface velocity clearly in-

<sup>9</sup> See Ref. 1, p. 248.